

Catalytic Pellet Reactor Under Uncertainty **Design**

**Final Presentation at the REU meeting
Chicago, IL, Tuesday, Aug. 4th, 2005.**

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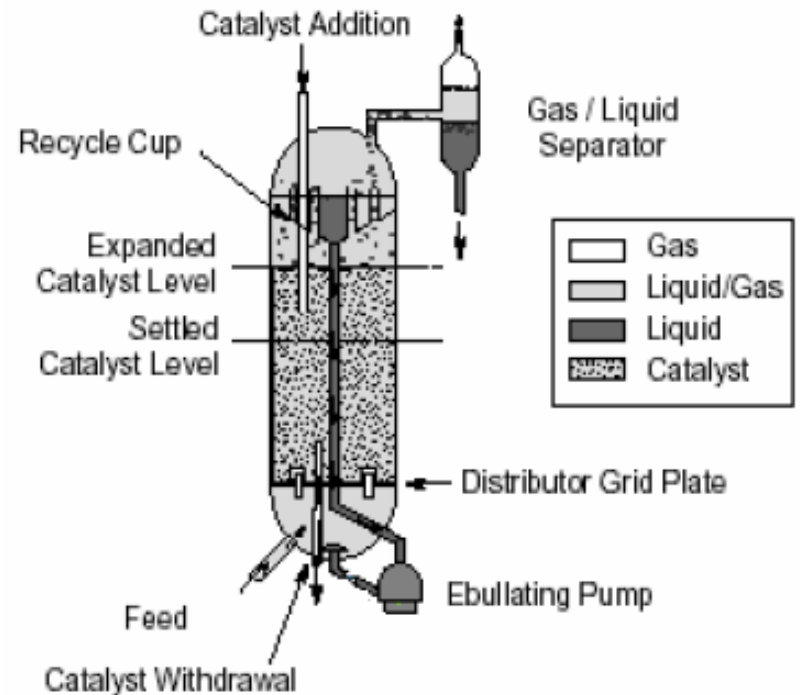
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Motivation

- **Catalytic Pellet Reactor**
- **Application:**
 - Catalytic Converters in cars
 - Paraffin Dehydrogenation
 - **Production of Sulfuric Acid**
- **Design Complication**
 - Coupling of Heat and Mass transfer phenomenon
 - **Impact of uncertain parameters**

Fig.1: A Typical Configuration of a Pellet Reactor



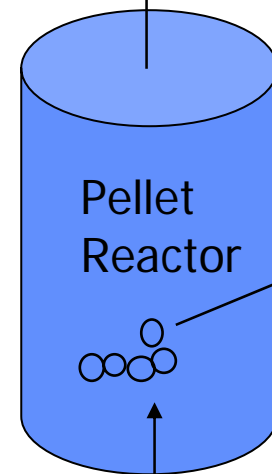
Design Under Uncertainty

- **Uncertain Parameter:**
 - system performance / safety
 - output quality.
- **Lack of understanding lead to:**
 - Loss of Revenue
 - **Unsafe Design (Hot Spot, Explosion etc.)**
- **Why we want to study it?**
 - Safety Condition
 - Guarantee product quality and maximum profit.
 - Control over design

Product Conversion??

Effectiveness Factor

Diffusion + Reaction



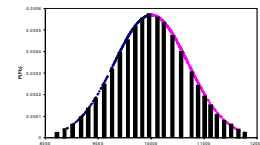
Property Uncertainty

Heat Conductivity: k_e

Mass Diffusivity: D_{ab}

Reaction rate: a

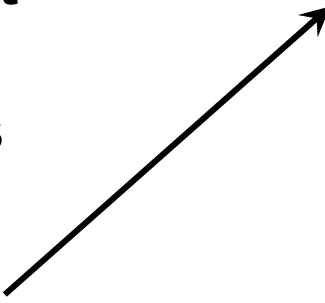
???



Operational Uncertainty

Methodology

- **Case Study: Pellet Reactor Design**
 - Develop Models
 - Solve Models in MATLAB
 - Analyze the system response
 - Quantify impact of uncertain parameters: safety, quality



- **Numerical Methods**
 - 1st Order ODE:
 - » R-K Method (ode45)
 - 2nd Order Differential Equation:
 - » Collocation Method
 - Integration:
 - » Adaptive Lobatto Quadrature Integration (quadl)

Case Study: Catalytic Pellet Reactor

• Catalytic Reaction:

- $\text{SO}_2(\text{g}) + 1/2 \text{O}_2(\text{g}) \leftrightarrow \text{SO}_3(\text{g})$
- 1st Order Heterogeneous reaction: $\text{A} \rightarrow \text{B}$

• Components of Design

- Pellets (T_s, C_s)
 - » Mass
 - » Energy
- Effectiveness Factor [Fogler]

$$\eta = \frac{\text{actual reaction rate}}{\text{reaction rate at surface}}$$
- Reactor (T_i, C_i)
 - » Mass
 - » Energy

Fig.2: Expanded View of a Pellet Reactor

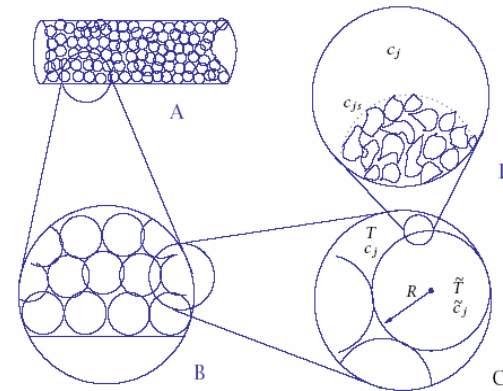


Fig. 3: Pellet Control Volume

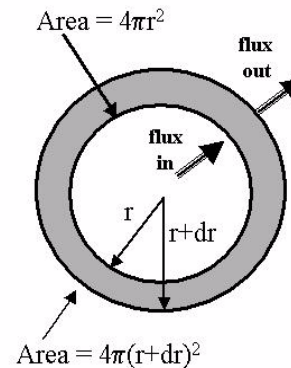
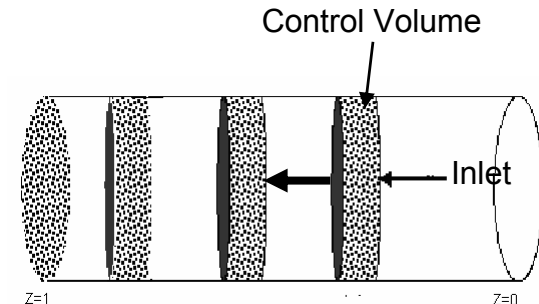


Fig. 4: Reactor Control Volume



Pellet Profiles

• Steady State

$$\frac{d^2 \phi}{d\theta^2} + \frac{2}{\theta} \frac{d\phi}{d\theta} - \Phi^2 \exp\left[\gamma\left(1 - \frac{1}{\zeta}\right)\right] \phi = 0$$

$$\frac{d^2 \zeta}{d\theta^2} + \frac{2}{\theta} \frac{d\zeta}{d\theta} - \beta \exp\left[\gamma\left(1 - \frac{1}{\zeta}\right)\right] \phi = 0$$

Boundary Conditions:

$$r=R: C_s, T_s$$

$$r=0: dC_s/dz=0, dT_s/dz=0$$

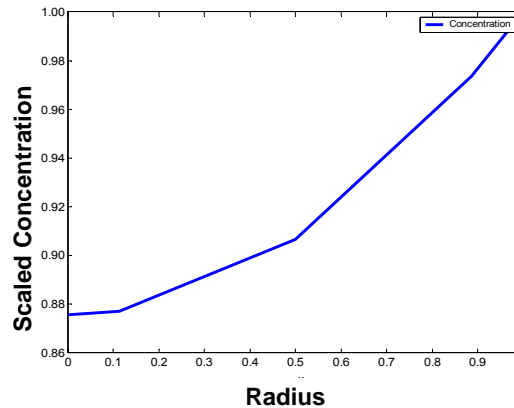
• Dynamic State

Initial Conditions:

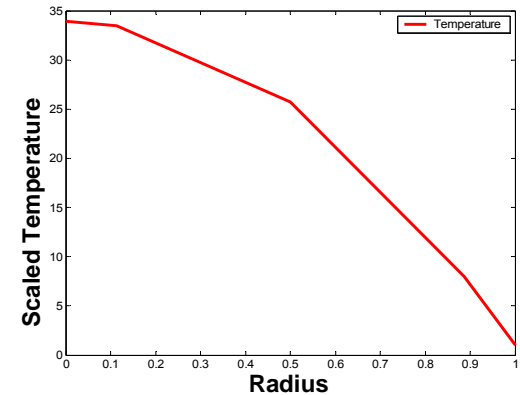
1. $t=0: T_0=1$

2. $t=0: C_0 = \text{Steady State result}$

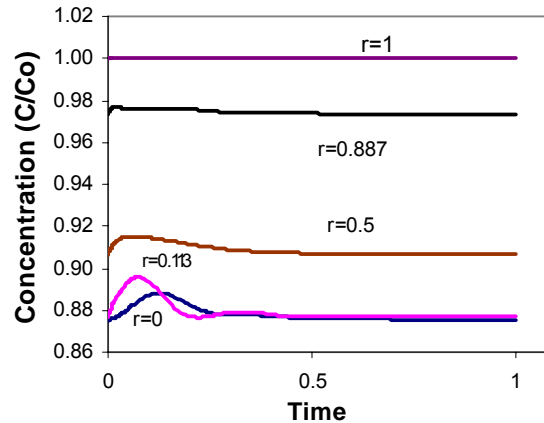
Steady State Pellet Concentration Profile



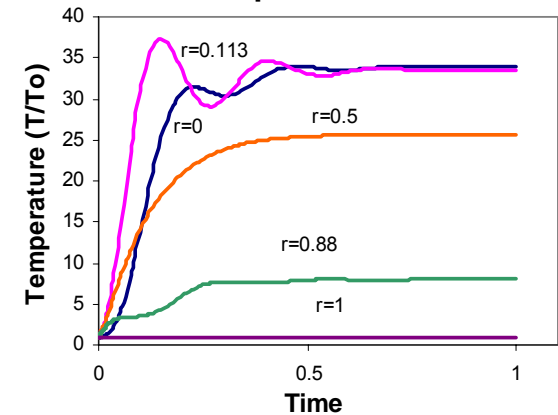
Steady State Pellet Temperature Profile



Dynamic Pellet Concentration Profile



Dynamic Pellet Temperature Profile

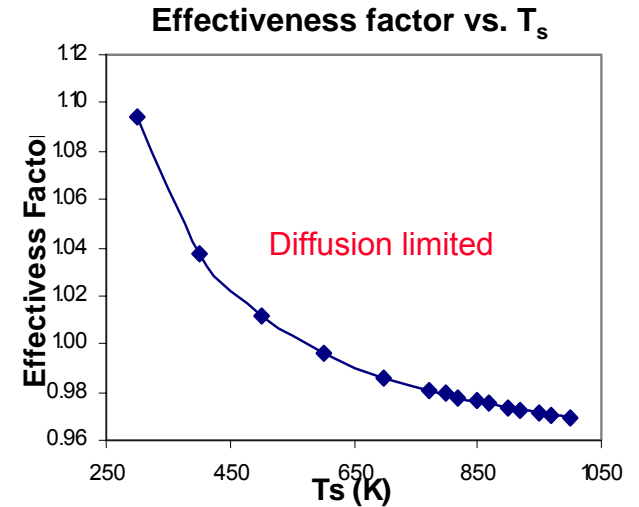
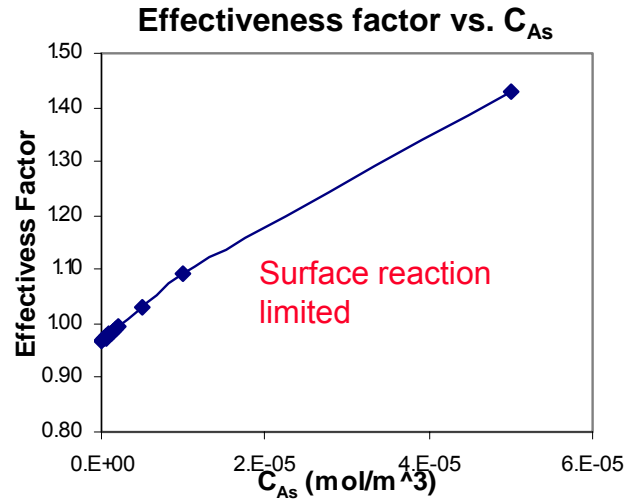


Pellet Sensitivity at Steady State

Nominal Values:

$$C_{As} = 2.46E-6 \text{ mol/m}^3$$

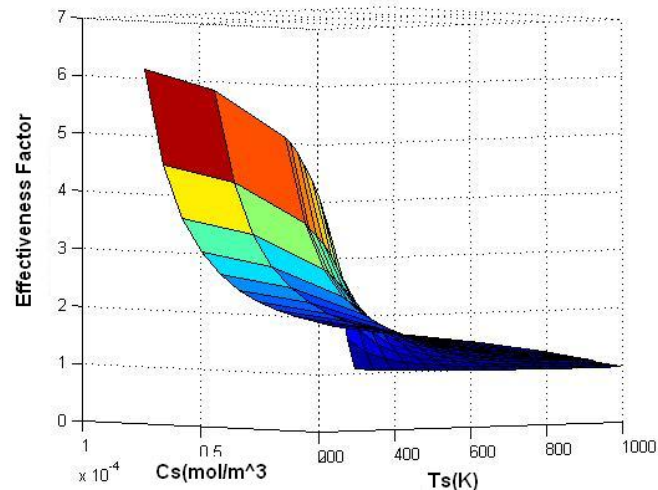
$$T_s = 550K$$



$$\eta = 3 \int_0^1 \varphi(\theta) \exp\left[\gamma\left(1 - \frac{1}{\xi}\right)\right] \theta^2 d\theta$$

$$\eta = \frac{\text{actual reaction rate}}{\text{reaction rate at surface}}$$

Effectiveness factor vs. Inlet conditions



Multiple Steady States for Pellets

Reaction Condition:

- Thiele Modulus = 0.430

$$\Phi^2 = \frac{R^2}{D_e} \left[a \exp\left(-\frac{E_a}{RT_s}\right) \right]$$

- Beta = 0.4 $\beta = \frac{(T_{\max} - T_s)}{T_s}$

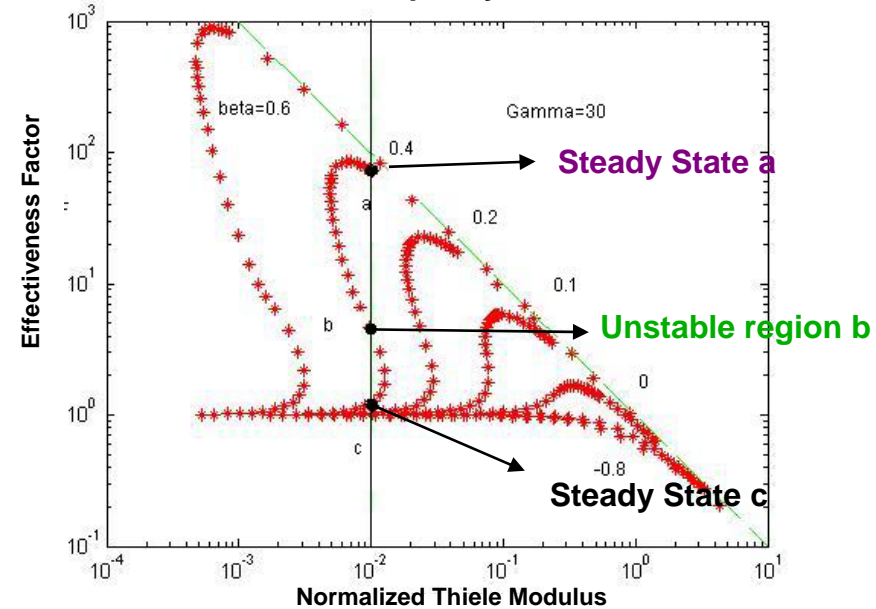
- Gamma = 30 $\gamma = \frac{E_a}{RT}$

Importance:

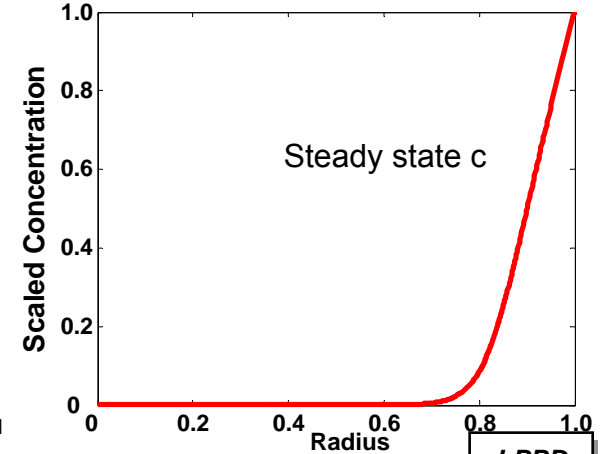
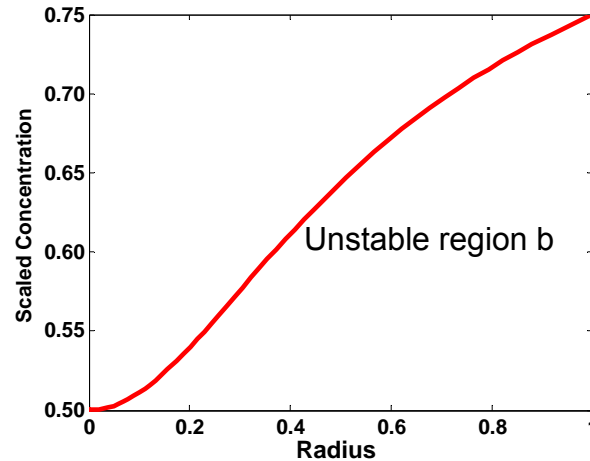
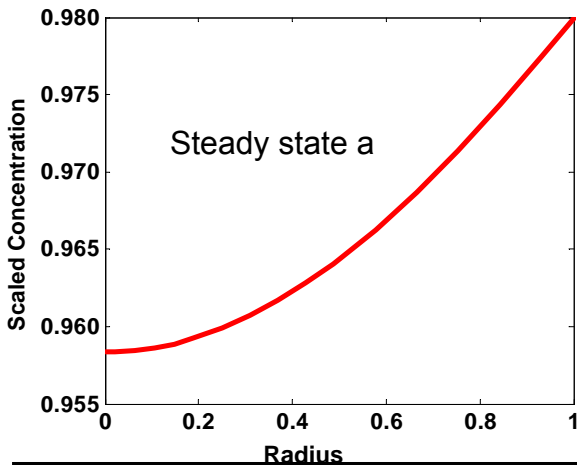
-- Initial Conditions

-- One steady state may go to another!!

Multiplicity



Concentration profiles for a single reaction condition



Reactor Profiles

Steady State:

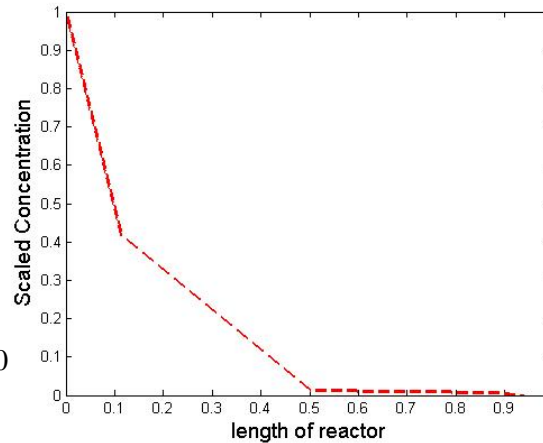
$$C_i = 1.6E-2 \text{ mol/m}^3$$

$$T_i = 300K$$

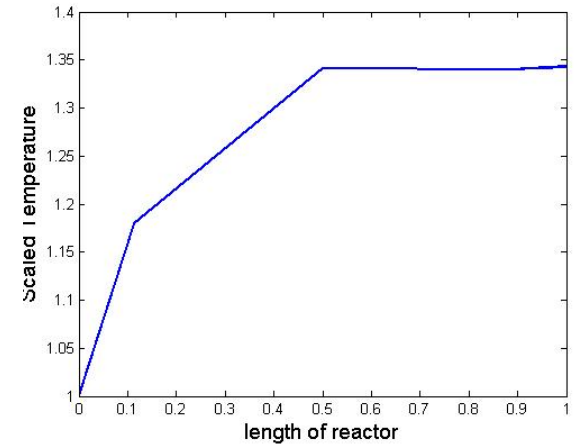
$$\frac{d^2 C_r}{dz^2} - \frac{U}{D_{AB}} \frac{dC_r}{dz} - \frac{\eta S_a k_o \rho_b}{D_{AB}} C_r \exp\left[\gamma\left(1 - \frac{1}{T_r}\right)\right] = 0$$

$$\frac{d^2 T_r}{dz^2} - \frac{\rho_g C_p U}{k_b} \frac{dT_r}{dz} - \frac{\Delta H \eta S_a C_i \rho_b}{k_b T_i} C_r \exp\left[\gamma\left(1 - \frac{1}{T_r}\right)\right] = 0$$

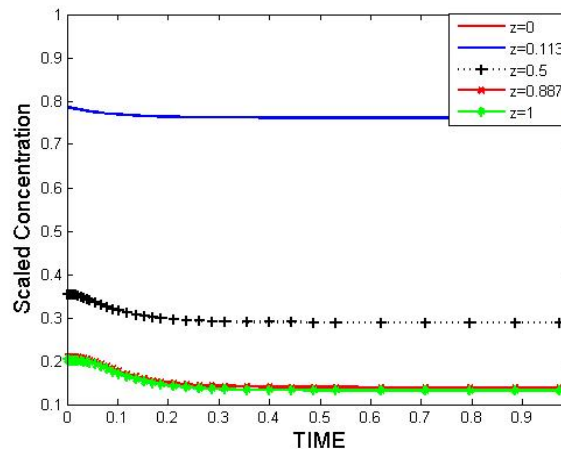
Steady State Concentration Profile



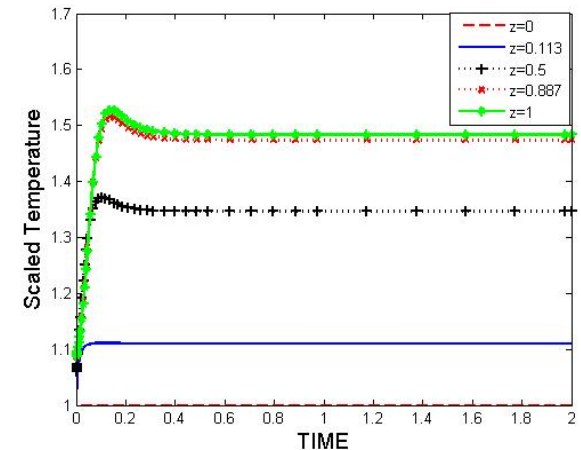
Steady State Temperature Profile



Dynamic Concentration Profile



Dynamic Temperature Profile



Dynamic State:

Initial Condition: Steady State

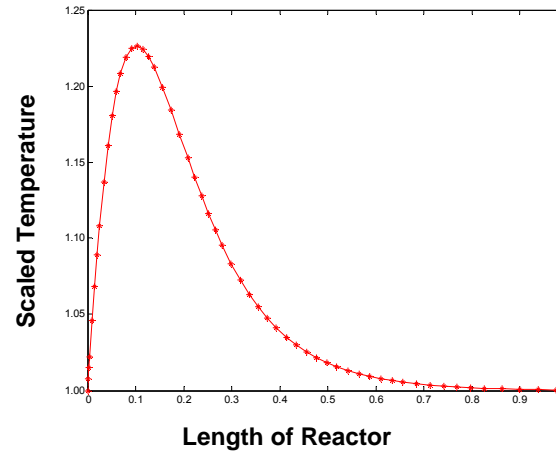
$$C_i = 1.6E-2 * 5 \text{ mol/m}^3$$

$$T_i = 300K$$

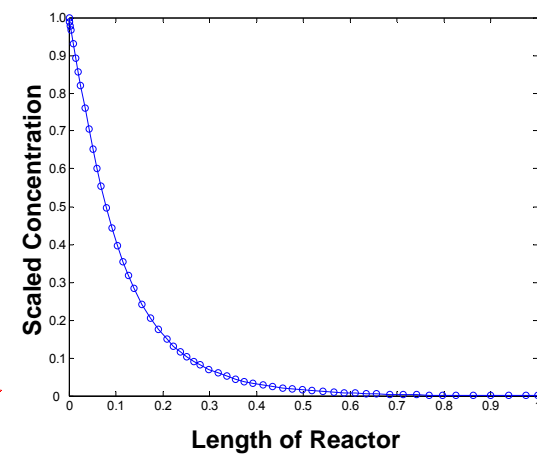
Reactor Safety: Hotspot

- **“Hotspot”** [Froment.] :
 - Temperature Profile reach a maximum
 - Very exothermic reaction
- **Why “hotspot” happens?**
 - Depletion of reactant
 - Cooling

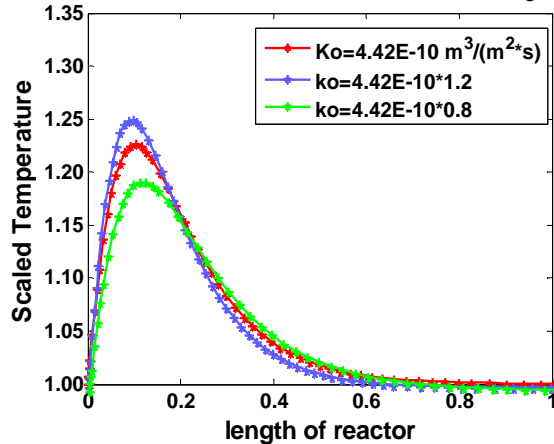
Temperature Profile



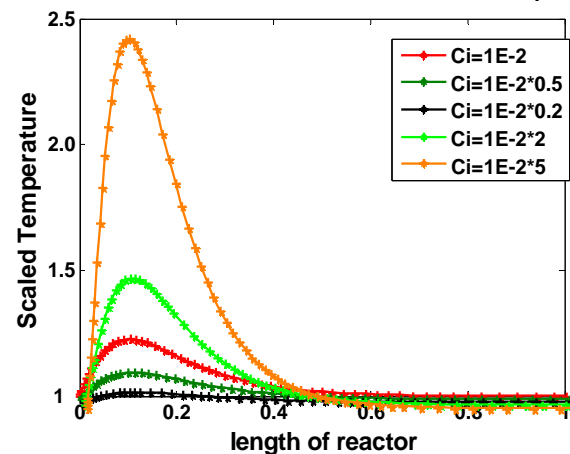
Concentration Profile



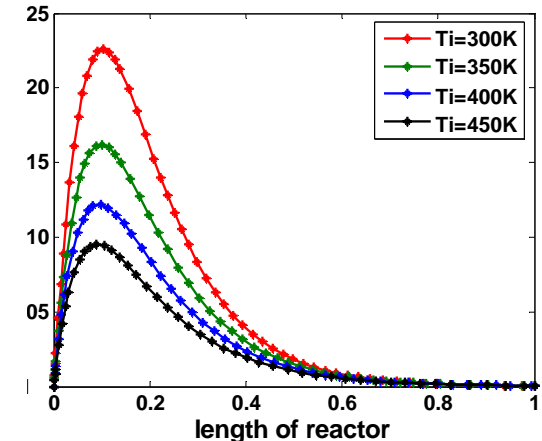
Temperature Profile vs. k_o



Temperature Profile vs. C_i



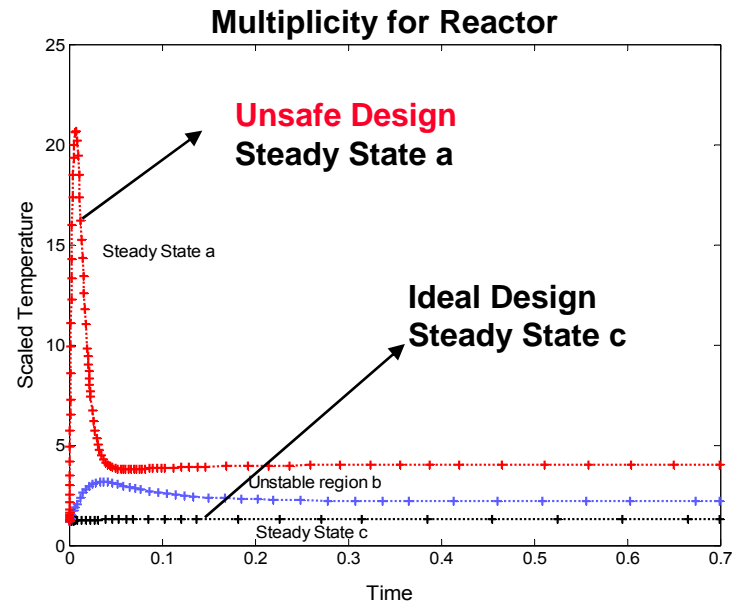
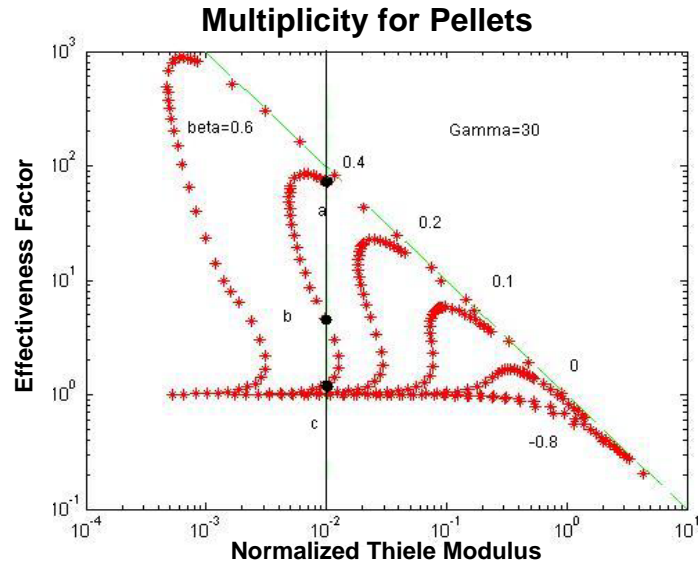
Temperature Profile vs. T_i



Reactor Safety: Multiplicity

- How does reactor respond to pellet multiplicity?
- **By testing uncertainty in inlet conditions, we find unsafe design!**

- Initial steady state ($z=0.5$)
 - » $T_r=1.2$
 - » $C_r=0.7$
- Disturbance:
 - » $T_i=300K$
 - » $C_i=1E-2 \text{ mol/m}^3$



Conclusion

- Pellet steady/dynamic state profiles
- Multiplicity in pellets
- Reactor steady/dynamic state profiles
- Reactor “hotspot”
- **Uncertainty analysis helps to prevent unsafe design!**

References

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- 5. Perkins Victor and Gomez Javier Cruz. *Assessment of Electricity Generation to 2011 Using Low Sulfur Fuel Oil in Mexico.*
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Acknowledgement

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